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LAMP DEVICE FOR VEHICLE

FIELD OF THE INVENTION

The present invention relates to a lamp device for
5 a vehicle, for example, a head lamp for a motor vehicle,
a fog lamp for a motor vehicle or the like which lights a
forward section of the motor vehicle. In particular, the
invention relates to a lamp device for a vehicle in which
a light distributing function is mainly given to a reflector
10 side.

BACKGROUND OF THE INVENTION

In a recent lamp device for a vehicle, a reflection
surface of a reflector is formed in a free curves surface
15 and a light distributing function is given to a side of the
reflector. Further, in the recent lamp device for the
vehicle, a so-called plain lens is used as a lens thereof
and a function of an outer cover is given to a side of the
lens. The plain lens corresponds to a lens in which a prism
20 for light distribution is not formed and the light transmits
as it is without being refracted. That is, the plain lens
is constituted by a light transmitting member formed in a
plate (a flat plate, a curved plate) shape such as a simple
plate glass or the like.

25 However, in the conventional lamp device for the

vehicle, the reflection surface of the internal reflector is clearly visible through the plain lens from an external section. Accordingly, it is necessary that the conventional lamp device for the vehicle is finished so as 5 to have at least an optical performance required for reflection on a surface of the reflection surface of the reflector, and this working operation is troublesome.

Accordingly, the inventors of this invention have invented a lamp device for a vehicle in which an interior 10 section is made hard to be visible in comparison with the plain lens (Japanese Patent Application No. 11-209331 (Japanese Patent Application Laid-Open No. 2001-35215)).

SUMMARY OF THE INVENTION

15 It is an object of this invention to provide a lamp device for a vehicle in which a surface finishing process of a reflection surface in a reflector can be easily executed than the conventional one by making an interior section hard to be viewed in comparison with a plain lens.

20 In order to achieve the object, according to one aspect of the present invention, there is provided the lamp device for a vehicle wherein, a shape of a vertical cross section and a shape of a horizontal cross section in a lens are convex shapes.

25 As a result, in accordance with the invention, since

the shape of the vertical cross section and the shape of the horizontal cross section in the lens have the convex shape, a light transmitting through the lens is largely reflected without a prism being formed, whereby the interior 5 section becomes hard to be viewed. Accordingly, in accordance with the invention, it is not necessary to finish the surface of the reflection surface of the reflector so as to have an optical performance equal to or more than an optical performance required for reflection with taking an 10 appearance into consideration, and the working operation can be easily executed in comparison with the conventional structure.

Other objects and features of this invention will become understood from the following description with 15 reference to the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a vertical cross sectional view which shows a summary of a head lamp for a motor vehicle in accordance 20 with an embodiment of the invention;

Fig. 2 is a horizontal cross sectional view;

Fig. 3 is a front elevational view;

Fig. 4 is a perspective view of a lens;

Fig. 5 is a front elevational view of a reflection 25 surface;

Fig. 6 is a flow chart showing a method of manufacturing the reflection surface;

Fig. 7A is a front elevational view for explanation showing a data input to an optical simulation;

5 Fig. 7B is a cross sectional view along a line B-B in Fig. 7A;

Fig. 7C is a cross sectional view along a line C-C in Fig. 7A;

Fig. 7D is an enlarged view of a section D in Fig. 10 7C;

Fig. 8A is an explanatory view which shows a representative light distribution pattern given by a pin point P_1 in Fig. 5 projected on a screen;

15 Fig. 8B is an explanatory view which shows a representative light distribution pattern given by a pin point P_2 in Fig. 5 projected on the screen;

Fig. 9 is an equiluminous curve showing a target distribution pattern of a low beam given by the head lamp for the motor vehicle in accordance with the first 20 embodiment;

Fig. 10 is an explanatory view of a light distribution pattern briefly showing a light distribution pattern obtained by a lens 1 shown in Figs. 1 to 4 and a first reflection surface block 21 from the left of the reflection surface 25 4 shown in Fig. 5, which is obtained in accordance with a

simulation of a computer;

Fig. 11 is an explanatory view of a light distribution pattern briefly showing a light distribution pattern obtained by the lens 1 shown in Figs. 1 to 4 and a second 5 reflection surface block 22 from the left of the reflection surface 4 shown in Fig. 5, which is obtained in accordance with the simulation of the computer;

Fig. 12 is an explanatory view of a light distribution pattern briefly showing a light distribution pattern 10 obtained by the lens 1 shown in Figs. 1 to 4 and a third reflection surface block 23 from the left of the reflection surface 4 shown in Fig. 5, which is obtained in accordance with the simulation of the computer;

Fig. 13 is an explanatory view of a light distribution 15 pattern briefly showing a light distribution pattern obtained by the lens 1 shown in Figs. 1 to 4 and a fourth reflection surface block 24 from the left of the reflection surface 4 shown in Fig. 5, which is obtained in accordance with the simulation of the computer;

20 Fig. 14 is an explanatory view of a light distribution pattern briefly showing a light distribution pattern obtained by the lens 1 shown in Figs. 1 to 4 and a fifth reflection surface block 25 from the left of the reflection surface 4 shown in Fig. 5, which is obtained in accordance 25 with the simulation of the computer;

Fig. 15 is an explanatory view of a light distribution pattern briefly showing a light distribution pattern obtained by the lens 1 shown in Figs. 1 to 4 and a sixth reflection surface block 26 from the left of the reflection 5 surface 4 shown in Fig. 5, which is obtained in accordance with the simulation of the computer; and

Figs. 16A, 16B and 16C are cross sectional views which show a modified embodiment of a convex shape corresponding to a cross sectional shape of the lens.

10

DETAILED DESCRIPTIONS

A description will be given below of an example of an embodiment of a lamp device for a vehicle in accordance with the invention with reference to the accompanying 15 drawings. In this case, the invention is not limited by the embodiment.

The embodiment explains a head lamp for a motor vehicle which can obtain a light distribution pattern of a low beam (a light distribution pattern for crossing). In this case, 20 the invention can be applied to the other lamp device for a vehicle. For example, the invention can be applied to a head lamp for a motor vehicle which can obtain a light distribution pattern of a high beam, a light distribution pattern for a high speed travel, a light distribution pattern 25 for an urban area travel and the like, a fog lamp for a motor

vehicle which can obtain a light distribution pattern for a dense fog, or the like.

The head lamp for the motor vehicle in accordance with the invention is equipped in a motor vehicle sectioned in 5 a left-hand traffic. Accordingly, in the case of a head lamp for a motor vehicle equipped in a motor vehicle sectioned in a right-hand traffic, right and left sections are reversed on the drawing.

The head lamp for the motor vehicle in accordance with 10 the embodiment is provided with a lens 1 arranged in a front surface of a lamp housing (not shown), a light source 2 and a reflector 3. In this case, reference symbol S denotes an optical axis.

The lens 1 is structured, as shown in Figs. 1 to 4, 15 such that an outer shape seen from a front surface is formed in a circular shape (may be formed in a rectangular shape), and a shape of a vertical cross section and a shape of a horizontal cross section are formed in a convex shape. A prism for light distribution is not formed in the lens 1. 20 A non-uniform rational B-spline surface (NURBS) corresponding to a free curved surface for light distribution is formed on a front surface and a back surface of the lens 1. The lens 1 may be made of a glass or a resin.

The light source 2 employs, for example, a halogen 25 lamp of a single filament or a double filament, an

incandescent lamp, an electric discharge lamp or the like (so-called H1, H3, H4, H7, H11 or the like).

A reflection surface 4 of the NURBS corresponding to the free curved surface for light distribution is formed 5 on an inner surface of the reflector 3. The reflection surface 4 takes on a high intensity feeling of a metal on the basis of an aluminum vapor deposition, a silver color painting or the like. The reflector 3 may be integrally formed with the lamp housing or independently formed 10 therefrom. Further, outer shapes of the reflector 3 and the reflection surface 4 seen from front surfaces thereof may be formed in a circular shape or a rectangular shape. Further, details of the reflection surface 4 of the NURBS are described, for example, in "Mathematical Elements for 15 Computer Graphics" (Devid F. Rogers, J Alan Adams).

That is, the reflection surface 4 of the NURBS in the case in which the front surface and the back surface use the lens 1 of the NURBS can be calculated in accordance with a general equation in the following equation (1).

$$20 \quad P(u, v) = \sum_{j=0}^m \sum_{k=0}^n P_{j,k} N_{j,s}(u) M_{k,t}(v) \quad \dots (1)$$

The reflection surface 4 of the NURBS calculated in accordance with the above equation (1) is structured such that the vertical cross section and the horizontal cross section are formed in a substantially hyperboloidal surface

(a surface similar to a hyperboloidal surface) smaller than the lens 1 as shown in Figs. 1 and 2.

A parametric function of the general equation in the above equation (1) is shown in the following equation (2).

5 A particular reflection surface 4 of the reflector 3 in the case of using the lens 1 can be obtained by substituting a particular numeric value, for example, a point on the hyperboloidal surface or the like for the parametric function in the following equation (2).

10
$$N_{j,s}(u) = \begin{cases} 1 & (\text{if } u_j \leq u < u_{j+1}) \\ 0 & (\text{the other cases}) \end{cases}$$

$$N_{j,s}(u) = \frac{u - u_j}{u_{j+s-1} - u_j} N_{j,s-1}(u) + \frac{u_{j+s} - u}{u_{j+s} - u_{j+1}} N_{j+1,s-1}(u)$$

$$M_{k,t}(v) = \begin{cases} 1 & (\text{if } v_k \leq v < v_{k+1}) \\ 0 & (\text{the other cases}) \end{cases}$$

15

$$M_{k,t}(v) = \frac{v - v_k}{v_{k+t-1} - v_k} M_{k,t-1}(v) + \frac{v_{k+t} - v}{v_{k+t} - v_{k+1}} M_{k+1,t-1}(v)$$

... (2)

An example of the particular reflection surface 4 obtained in the manner will be shown in Fig. 5. The 20 reflection surface 4 in this one example is vertically separated into six pieces. Boundary lines (joint lines)

of these six separated reflection surface blocks (or reflection surface segments) 21, 22, 23, 24, 25 and 26 (21 to 26) include a type in which the reflection surface blocks 21 to 26 are independently visible as shown, and a type in 5 which the reflection surface blocks 21 to 26 are not continuously visible.

In this case, the reflection surface 4 shown in Fig. 5 corresponds to one example in which the reflection surface blocks are separated in a vertical direction. Therefore, 10 in accordance with the invention, the reflection blocks may be separated in a horizontal direction, separated in a radial direction or separated in the vertical direction, the horizontal direction and the radial direction in a suitably combined manner. That is, the reflection surface blocks 15 may be separated with taking a design thereof into consideration.

In this case, since the reflection surface 4 is structured such that the reflection surfaces of the NURBS are combined in a composite manner, a single optical axis 20 in the strict sense is not provided in the optical axis S of the reflection surface 4, however, a difference among a plurality of optical axes is slight, and substantially the same optical axis is commonly used. Accordingly, in this specification and the drawings, the substantially same 25 optical axis is called as an artificial optical axis (or

simply an optical axis) S. In the same manner, in a focus F of the reflection surface 4 (refer to Fig. 7C), a single optical axis in the strict sense is not provided, however, a difference among a plurality of optical axes is slight, 5 and substantially the same optical axis is commonly used. Accordingly, in this specification and the drawings, the substantially same optical axis is called as an artificial optical axis (or simply an optical axis).

A description will be given below of an example of 10 a method of manufacturing the reflection surface 4 with reference to Fig. 6.

At first, in a step 1 (S1), a data is input to a microcomputer (not shown). The data is selected among a design specification and the like in a data base with taking 15 a design of a head lamp for a motor vehicle and a design of the motor vehicle mounting the head lamp for the motor vehicle thereon. The data includes a kind of the light source 2, a size of the reflector 3, a front surface shape of the reflection surface 4, a separation of the reflection surface 20 blocks 21 to 26, a size, a front surface shape and a back surface shape of the lens 1, a target light distribution pattern and the like.

In a step 2 (S2), there is executed a process of temporarily setting the reflection surface of the reflector 25 in accordance with a combination with a planar lens on the

basis of the data input in the step 1 so that the target light distribution pattern can be obtained. The reflection surface of the temporarily set reflector is automatically set on the basis of a control point on the free curved surface 5 of the NURBS, a normal vector and the like.

In a step 3 (S3), there is executed a process of changing the planar lens to the lens 1 in which the vertical cross section and the horizontal cross section are formed in the convex shape, without changing the reflection surface of 10 the temporarily set reflector obtained in accordance with the process in the step 2. At this time, in accordance with a ray tracing method, a light distribution pattern (not shown) of an image which is formed by a process in which the light output from the modeled light source 2 is reflected 15 on the reflection surface of the reflector, and the reflected light is refracted by the lens and thereafter reaches on a forward screen (not shown) as an outgoing light, can be obtained by a calculation.

In a step 4 (S4), there is executed a process of 20 calculating a difference between the target light distribution pattern obtained in accordance with the process in the step 2 and the light distribution pattern obtained in accordance with the process in the step 3. This difference is generated by a refraction of the light in the lens 1.

25 In a step 5 (S5) and a step 6 (S6), there is executed

a process of formally setting the reflection surface of the temporarily set reflector to the reflection surface 4 of the reflector 3 for the lens 1 so that the difference calculated in accordance with the process in the step 4 5 becomes 0. That is, an optimum free curved surface of the NURBS is formed by automatically correcting and deforming the free curved surface of the NURBS on the reflection surface so that the light distribution pattern obtained in accordance with the process in the step 3 becomes the target light 10 distribution pattern obtained in accordance with the process in the step 2. The processes in the step 5 and the step 6 corresponds to a process of repeating a ray tracing calculation in which the light output from the light source 2 is reflected on the reflection surface 4 of the reflector 15 3, and the reflected light is refracted by the lens 1 and thereafter reaches on the forward screen (not shown) as the outgoing light beam, in accordance with the ray tracing method.

When the difference becomes substantially 0, it is 20 assumed that the reflection surface 4 of the reflector 3 for the lens 1 is formerly set, and in a step 7 (S7), the reflection surface 4 of the formerly set reflector 3 is output.

As mentioned above, in this manufacturing method, it 25 is possible to manufacture the reflection surface 4 of the

NURBS in the case of using the lens 1 in which the front surface and the back surface are the NURBS. Further, by executing the processes in the steps 2 to 6, that is, the temporarily setting step of the reflection surface of the 5 reflector 3, the difference calculating step, and the formerly setting step of the reflection surface 4 of the reflector 3 in accordance with a predetermined program by a computer, it is possible to manufacture the reflection surface 4 at a high accuracy, a high speed and a high degree 10 of freedom.

A description will be given in detail of a result obtained by executing a trial an optical design simulation of the head lamp for the motor vehicle in accordance with this embodiment. Figs. 7A to 7D are explanatory views which 15 show a data input to the optical design simulation. Data sizes in Figs. 7A to 7D are respectively as follows.

$A_r = 100$ mm (horizontal size of the reflector 3)

$B_r = 100$ mm (vertical size of the reflector 3)

$A_l = 160$ mm (horizontal size of the lens 1)

20 $B_l = 160$ mm (vertical size of the lens 1)

$T = 28$ mm (thickness size of the lens 1 (in the optical axis S))

$S_v = 0$ degree (angle of incline of side surface in the lens 1 (in the optical axis S))

25 $S_h = 0$ degree (angle of incline of plane surface in the lens

1 (in the optical axis S))
Rvo = - 300 mm (radius of curvature in the side surface optical
axis S of front surface in the lens 1)
Rho = - 300 mm (radius of curvature in the plane surface
5 optical axis S of front surface in the lens 1)
Rvi = 200 mm (radius of curvature in the side surface optical
axis S of back surface in the lens 1)
Rhi = 200 mm (radius of curvature in the plane surface optical
axis S of back surface in the lens 1)
10 F = 22 mm (focal distance)
Lf = 4.6 mm (length of filament of the light source 2)
Rf = 0.73 mm (radius of filament of the light source 2)
The data is input to values in Table 1 described below. In
this case, a condition is made so that an European Light
15 Distribution Regulation ECE Reg. is satisfied.

Table 1

Reflector 3		
Horizontal	Vertical	Focal distance
Ar (mm)	Br (mm)	F (mm)
100	100	20

When lighting the light source 2 of the head lamp for

the motor vehicle in accordance with the embodiment, the following result in Table 2 will be obtained.

Table 2

5

European Light Distribution Regulation	Satisfaction
Maximum light intensity (cd)	24800
Use light intensity (lm)	408
Light generating section (mm)	Vertical
	Horizontal
	Thickness

In the head lamp for the motor vehicle in accordance with this embodiment, the light source 2 is turned on. Then, 10 as shown in Figs. 1 and 2, a light L_1 output from the light source 2 is reflected on the reflection surface 4 of the reflector 3, and the reflected lights L_2 and L_3 are irradiated outward as outgoing lights L_4 and L_5 via the lens 1 on the

basis of a target light distribution pattern shown in Fig. 9. The target light distribution pattern corresponds to a light distribution pattern proper to a light distribution regulation such as European Light Distribution Regulation 5 ECE Reg. or a regulation based thereon (for example, Japan Domestic Model Certified Regulation), North America Light Distribution Regulation, FMVSS or the like.

The target light distribution pattern shown in Fig. 9 corresponds to a light distribution pattern of a low beam 10 sectioned in a left-hand traffic, and is controlled by the respective reflection surface blocks 21 to 26 of the reflection surface 4 in the reflector 3. That is, in the reflection surface 4 of the reflector 3 shown in Fig. 5, a light distribution pattern shown in Fig. 10 is controlled 15 and obtained in a first reflection surface block 21 from the left, a light distribution pattern shown in Fig. 11 is controlled and obtained in a second reflection surface block 22 from the left, a light distribution pattern shown in Fig. 12 is controlled and obtained in a third reflection surface 20 block 23 from the left, a light distribution pattern shown in Fig. 13 is controlled and obtained in a fourth reflection surface block 24 from the left, a light distribution pattern shown in Fig. 14 is controlled and obtained in a fifth reflection surface block 25 from the left, and a light 25 distribution pattern shown in Fig. 15 is controlled and

obtained in a sixth reflection surface block 26 from the left, respectively. By combining the light distribution pattern (Figs. 10 to 15) controlled and obtained by the respective reflection surface blocks 21 to 26, the target
5 light distribution pattern shown in Fig. 9 is obtained.

As is apparent from Figs. 10 to 15, in the first, second and sixth reflection blocks 21, 22 and 26 from the left, since they are apart from the light source 2, the reflected light is weak. Accordingly, in these reflection blocks 21,
10 22 and 26, a hot zone is formed by collecting the weak reflected lights. Therefore, the reflection surfaces of the reflection blocks 21, 22 and 26 are mainly formed in a recessed surface shape.

On the contrary, in the third to fifth reflection blocks
15 23 to 25 from the left, since they are close to the light source 2, the reflected light is strong, so that the strong reflected light simply forming a spot light is diffused. Accordingly, the reflection surfaces of the reflection blocks 23 to 25 are mainly formed in a convex surface shape.

20 In this case, in a design of a theoretical reflection surface 4, the light source 2 is prepared as a point light source, however, since the actual light source 2 has the length and the width (the radius) of the filament as is apparent from Figs. 1 and 2, it is not the point light source
25 but a surface light source.

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Accordingly, for example, as shown in Fig. 5, when the light of the light source 2 is reflected at one point P_1 on the reflection surface 4 in the third reflection surface block 23 from the left which is closest to the light source 5 2, the outgoing light L_5 output from a rear end b of the light source (filament) 2 is emitted to a lower side at an angle θ_1 with respect to a horizontal line S_1 , as shown in Fig. 1. On the contrary, the outgoing light L_4 output from a front end a of the light source (filament) 2 is emitted 10 to a lower side at an angle θ_2 with respect to the horizontal line S_1 . The emitted lights L_4 and L_5 are formed in a longitudinal shape in a vertical direction substantially in a center section on the screen, as shown in Figs. 8A and 12. Further, they are slightly inclined from the light 15 source 2 at a difference in the lateral direction. The angles θ_1 and θ_2 of the outgoing lights L_4 and L_5 emitted from the lens 1 with respect to the horizontal line S_1 are the same as the angle θ_1 and θ_2 on the screen from a horizontal line H-H, as shown in Fig. 8A.

20 For example, as shown in Fig. 5, when the light of the light source 2 is reflected at one point P_2 on the reflection surface 4 in the sixth reflection surface block 26 from the left, the outgoing light L_5 output from the rear end b of the light source (filament) 2 is emitted to an inner 25 side at an angle θ_3 with respect to a vertical line S_2 , as

shown in Fig. 2. On the contrary, the outgoing light L_4 output from the front end a of the light source (filament) 2 is emitted to an inner side at an angle θ_4 with respect to the vertical line S_2 . The emitted lights L_4 and L_5 are 5 formed in a longitudinal shape in a lateral direction in a left side of the substantially center section on the screen, as shown in Figs. 8B and 10. The angles θ_3 and θ_4 of the outgoing lights L_4 and L_5 emitted from the lens 1 with respect to the vertical line S_2 are the same as the angle θ_3 and θ_4 10 on the screen from a vertical line V-V, as shown in Fig 8B.

As mentioned above, the free curved surface formed on the reflection surface 4 is formed by simulating the light distribution pattern generated by the free curved surface by the computer so as to analyze a light distribution property, 15 thereby obtaining an optimum light distribution pattern. Accordingly, the light distribution pattern of the outgoing lights L_4 and L_5 at a time when the reflected light L_2 and L_3 generated by the reflection surface 4 pass through the lens 1 so as to be irradiated outward is optimum. Further, 20 in this embodiment, since the free curved surface (NURBS) is formed on the front surface and the back surface of the lens 1, the light distribution function can be given not only to the reflection surface 4 but also the lens 1, whereby a more ideal light distribution pattern can be obtained.

25 In particular, since the head lamp for the motor vehicle

in accordance with this embodiment is structured such that the vertical cross section and the horizontal cross section of the lens 1 are formed in the convex shape, the light is largely refracted by the lens 1 and the interior section 5 is hard to be visible in the case of being seen from the exterior section, even when the prism is not formed. Accordingly, in the head lamp for the motor vehicle in accordance with this embodiment, it is not necessary to finish the surface of the reflection surface 4 of the 10 reflector 3 so as to have the optical performance equal to or more than the optical performance required for reflection with taking the appearance into consideration, and the working operation can be easily executed in comparison with the conventional one.

15 The lens 1 in accordance with this embodiment is structured such that the shape of the vertical cross section and the shape of the horizontal cross section are formed in the convex shape. Accordingly, in the vertical and horizontal sections of the lens 1, as shown in Figs. 1 and 20 2, the lights L_2 and L_3 diffused by the substantially hyperboloidal surface of the reflection surface 4 are focused in the direction substantially extending along the optical axis S, and are irradiated to the external section on the basis of the target light distribution pattern. As a result, 25 in the embodiment, it is possible to construct the head lamp

for the motor vehicle in which the light generation area is large and the reflector 3 is small. Accordingly, the embodiment is preferably employed in the case of a vehicle body design in which a large placing space can not be 5 sufficiently secured in an inner section of a front section to which the head lamp for the motor vehicle should be mounted, particularly in the case of a compact car.

The reflection surface 4 in accordance with this embodiment is structured such that the vertical cross section 10 and the horizontal cross section are formed in the substantially hyperboloidal surface smaller than the lens 1. Accordingly, in the vertical cross section and the horizontal cross section of the reflection surface 4, as shown in Figs. 1 and 2, the lights L_2 and L_3 can be introduced 15 into the lens 1 in a state of being diffused vertically and horizontally with respect to the optical axis S . As a result, in this embodiment, the vertical cross section and the horizontal cross section are optimum for the combination with the lens 1 formed in the convex shape, and as shown 20 in Fig. 3, it is possible to easily obtain the head lamp for the motor vehicle in which the placing space of the inner section of the front surface (the lens 1 surface) can not be sufficiently secured.

In this case, in this embodiment, the convex shape 25 of the vertical cross section and the horizontal cross

section of the lens 1 means a shape having an optical function which refracts the incident light in a direction moving apart (diffusing) from the optical axis S, on the vertical cross surface of the lens 1. Accordingly, the convex shape 5 includes a shape in which only one surface is formed in a convex shape as shown in Fig. 16A, a shape in which one surface is formed in a recess surface and another surface is formed in a convex surface in more degree as shown in Fig. 16B, a shape in which the lens is arranged in an inclined manner 10 with respect to the optical axis S as shown in Fig. 16C, and the like.

In this embodiment, the NURBS corresponding to the free curved surface for light distribution is formed on the front surface and the back surface of the lens 1. However, 15 in this invention, a free curved surface or a torus curved surface for light distribution other than the NURBS may be formed on the front surface and the back surface of the lens 1.

In this invention, the NURBS, the free curved surface 20 or the torus curved surface corresponding to the free curved surface for light distribution may be formed on any one of the front surface and the back surface of the lens 1.

In this invention, the NURBS, the free curved surface or the torus curved surface corresponding to the free curved 25 surface for light distribution may not be formed on the front

surface and the back surface of the lens 1.

Although the invention has been described with respect to a specific embodiment for a complete and clear disclosure, the appended claims are not to be thus limited but are to 5 be construed as embodying all modifications and alternative constructions that may occur to one skilled in the art which fairly fall within the basic teaching herein set forth.